

## URTEC-198210-MS

# Optimisation of Dewatering Rates to Maximise Coal Seam Gas Production

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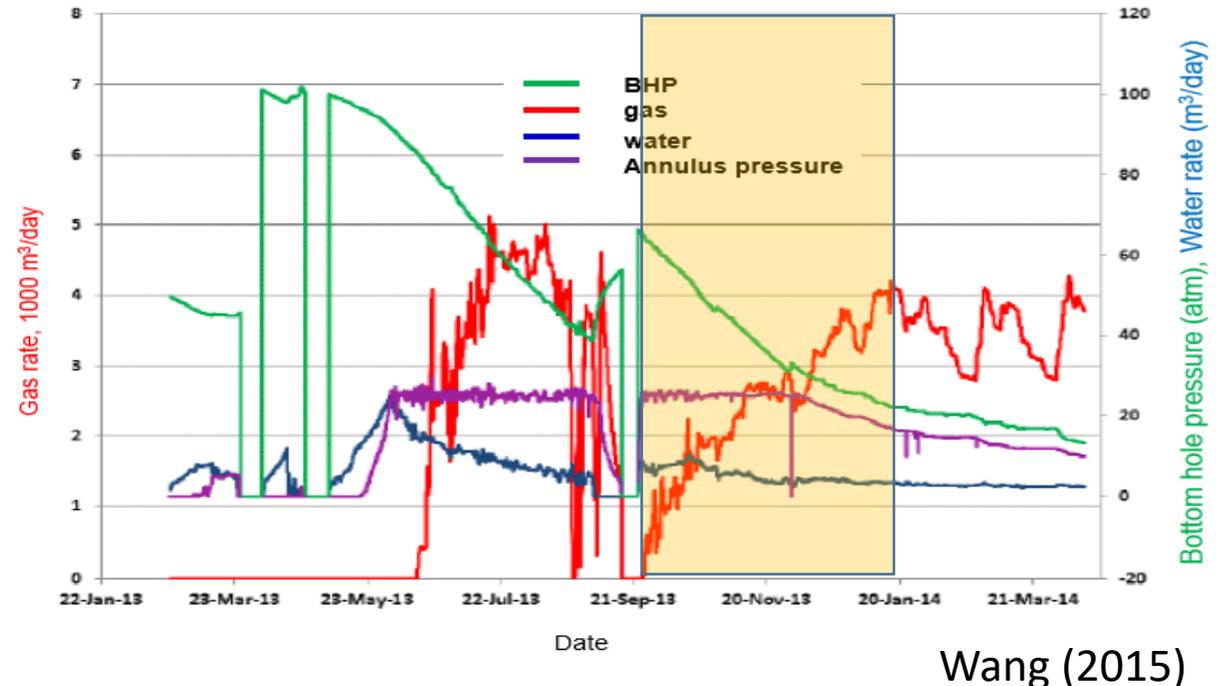
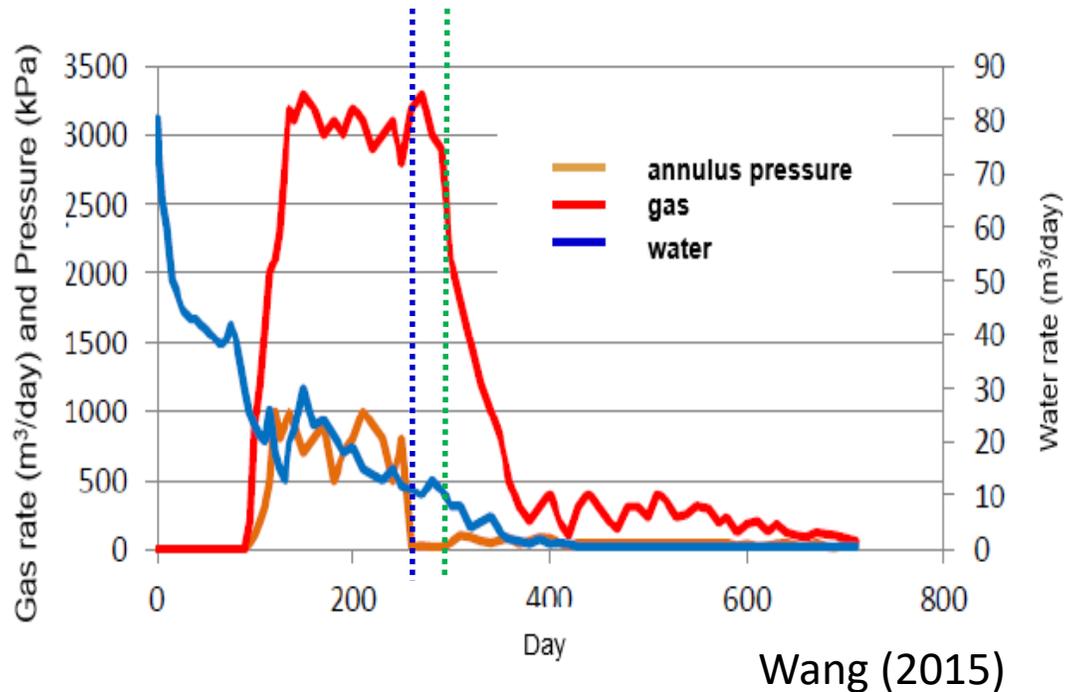
# Outlines

- ✓ Background
- ✓ Objectives and Methodology
- ✓ Model Implementation and Simulation Scenarios
- ✓ Results and Discussion
- ✓ Conclusions

# Background

The impact of dewatering rate on CSG productivity has been reported.

Reduction in BHP too quickly may dramatically reduce gas peak rate in the short term and reduce total production in the long term.



# Background

Possible reasons are:

1. Fluid pressure in cleats near wellbore decreases sharply, effective stress exerted upon the cleats increases and results in absolute permeability reduction
2. Early two-phase flow occurrence around the wellbore provides internal pressure maintenance and decreases the relative permeability to water
3. Other factors: wellbore stability and blockage of coal fines etc.

These, in turn, limit significant pressure propagation, limit desorption area and constrain water flow toward the well far from the fields.

# Objectives and Methodology

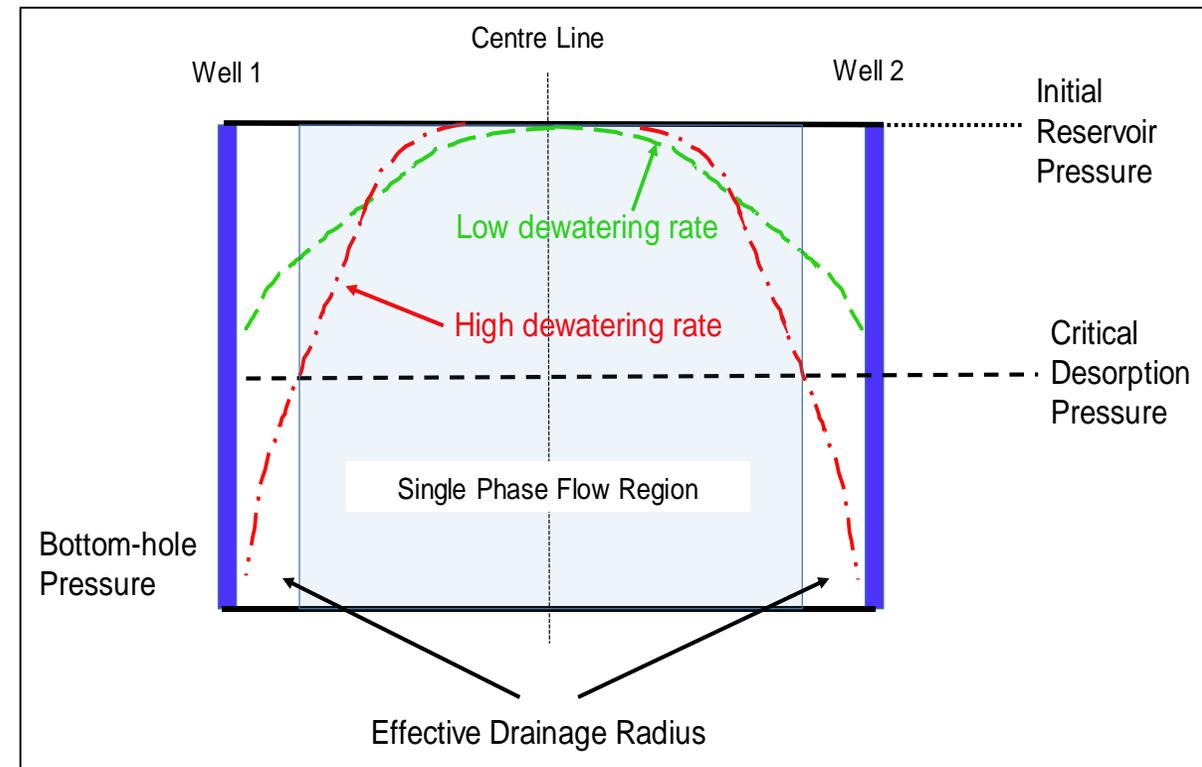
## ❖ Objectives

Investigate whether or/and how the Bottom-hole pressure (BHP) needs to be managed to maximise gas production from different CSG reservoir conditions.

## ❖ Methodology

Develop a 2D numerical model to evaluate the sensitivity of coal perm to relative perm curves and coal matrix shrinkage under different stress conditions, e.g., constant volume, constant stress and uniaxial strain.

For each case, separately simulate production behaviour under (i) **various drawdown strategies**, (ii) accounting for different relative permeability characteristics, (iii) **geo-mechanical properties** and (iv) isotherm properties.



# Model Implementation

## ❖ Model Geometry and Reservoir Condition

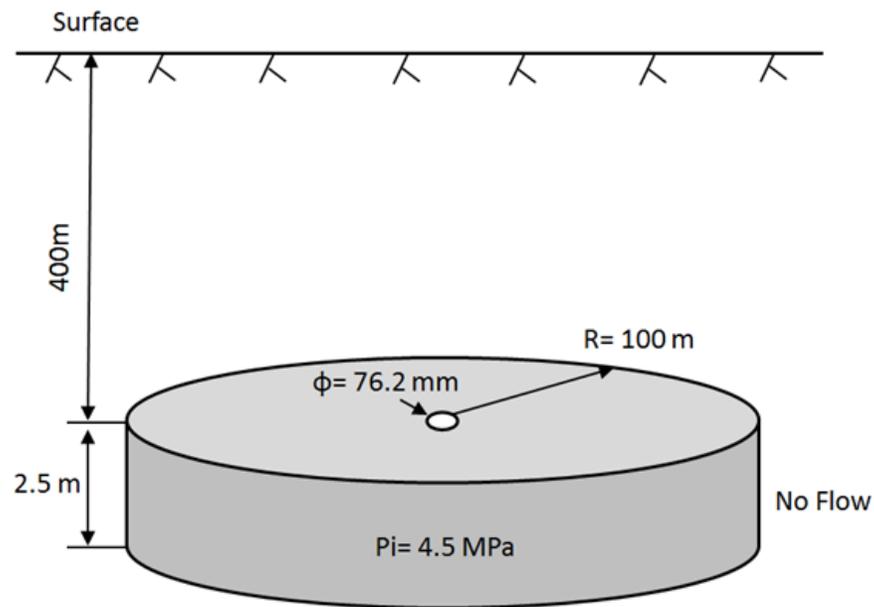


Illustration of numerical model geometry. The compositional simulator GEM from the Computer Modelling Group (CMG) suite was used. The radial grid system has **100 grid cells** in the **radial direction**, **3 grid cells** in the **angular direction** and **1 grid cell** (layer) in the **vertical direction**, making a **total of 300 grid cells** in the model.

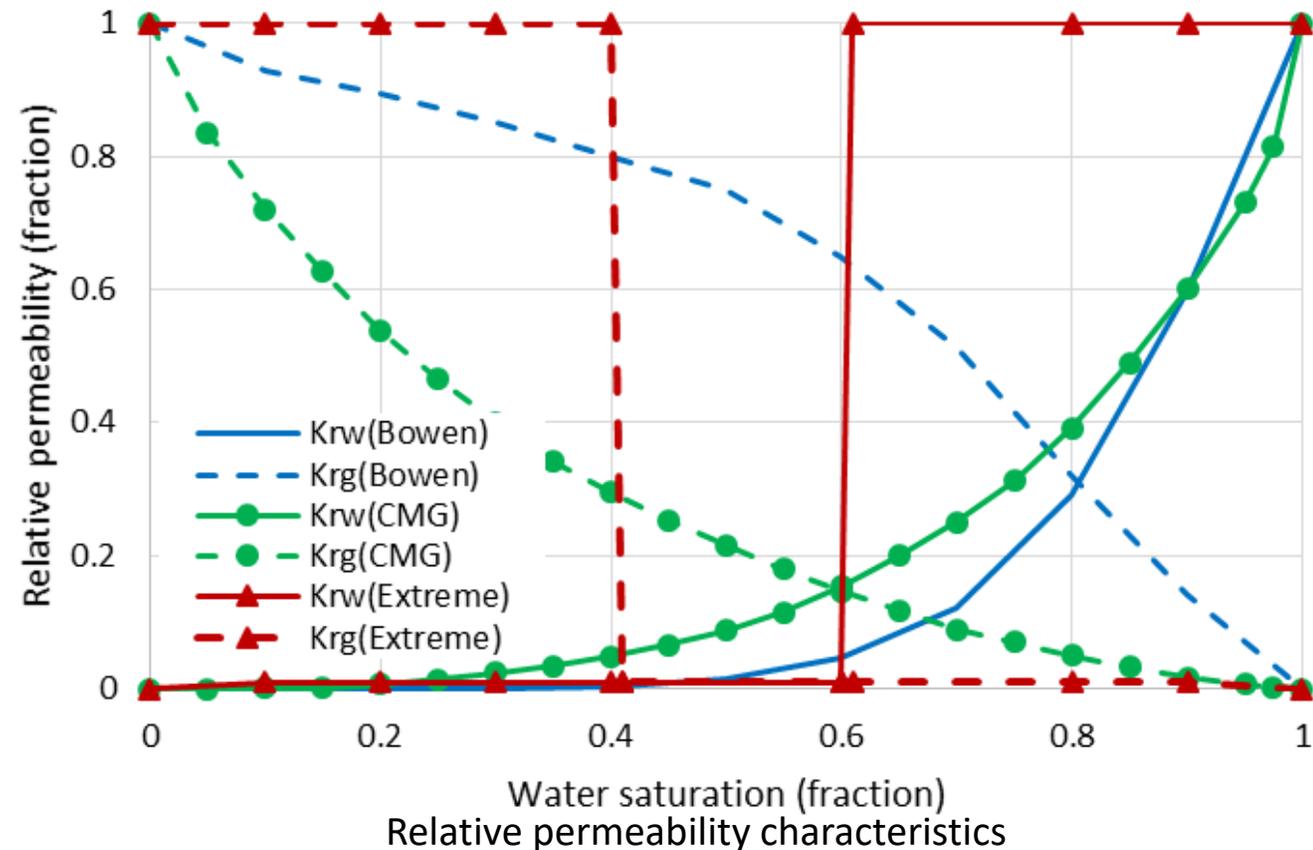
**Table:** Initial reservoir properties

Input	Value
Radius (m)	100
Thickness (m)	2.5
Reservoir depth (m)	450
Reservoir pressure (kPa)	4500
Reservoir temperature (°C)	40
Coal compressibility (1/kPa)	$2 \times 10^{-5}$
Horizontal fracture permeability (mD)	2
Vertical fracture permeability (mD)	2
Matrix porosity (fraction)	0.01
Fracture porosity (fraction)	0.005
Fracture spacing (m)	0.2
diffusion coefficient (cm <sup>2</sup> /s)	$2 \times 10^{-8}$
Coal density (kg/m <sup>3</sup> )	1400
Water density (kg/m <sup>3</sup> )	1000
Water viscosity (cp)	0.6

# Model Implementation

## ❖ Relative Permeability Characteristics

- For a real coal example, **blue curves** data published by *Meaney and Paterson (1996)*, determined by history match production data from German Creek Seam in Bowen Basin.
- As an intermediate case, **green curves** are specifically used by CMG for coal seam gas reservoir modelling.
- An idealised case, **red curves** represent an extreme hypothetical relative permeability case to investigate effects of jamming fluid flow in the reservoir.



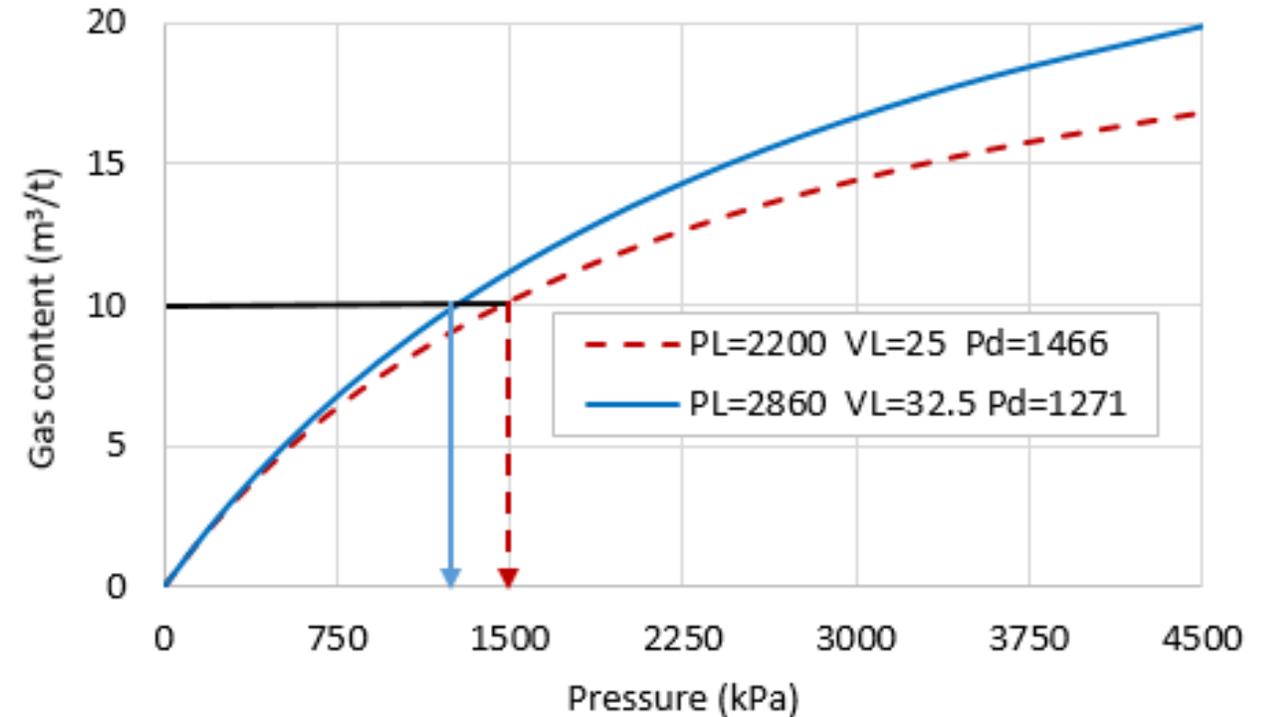
# Model Implementation

## ❖ Langmuir Isotherm and Geomechanical Properties

- Values in the Table below are related to coal seams from Bowen Basin and were obtained from core samples and history matched data (*Connell et al 2013, Mazumder et al 2012, Jeffery et al 1995, Morales et al 1993*).
- The two extreme values are within 30% of the mean values.

Geomechanical properties

Parameters	Low	Mean	High
Young's Modulus, $E$ (MPa)	2,072	2,800	3,528
Poisson's Ratio, $\nu$	0.26	0.35	0.44
Sorption-induced Strain, $\epsilon$	0.0089	0.0120	0.0151



Shows the Langmuir isotherm curves. The **red isotherm curve** ( $V_L$  and  $P_L$ ) is based on Bowen datasets (unpublished data). The **blue curve** has 30% higher  $V_L$  and  $P_L$ . Both curves were calculated with gas content  $GC=10 \text{ m}^3/\text{t}$

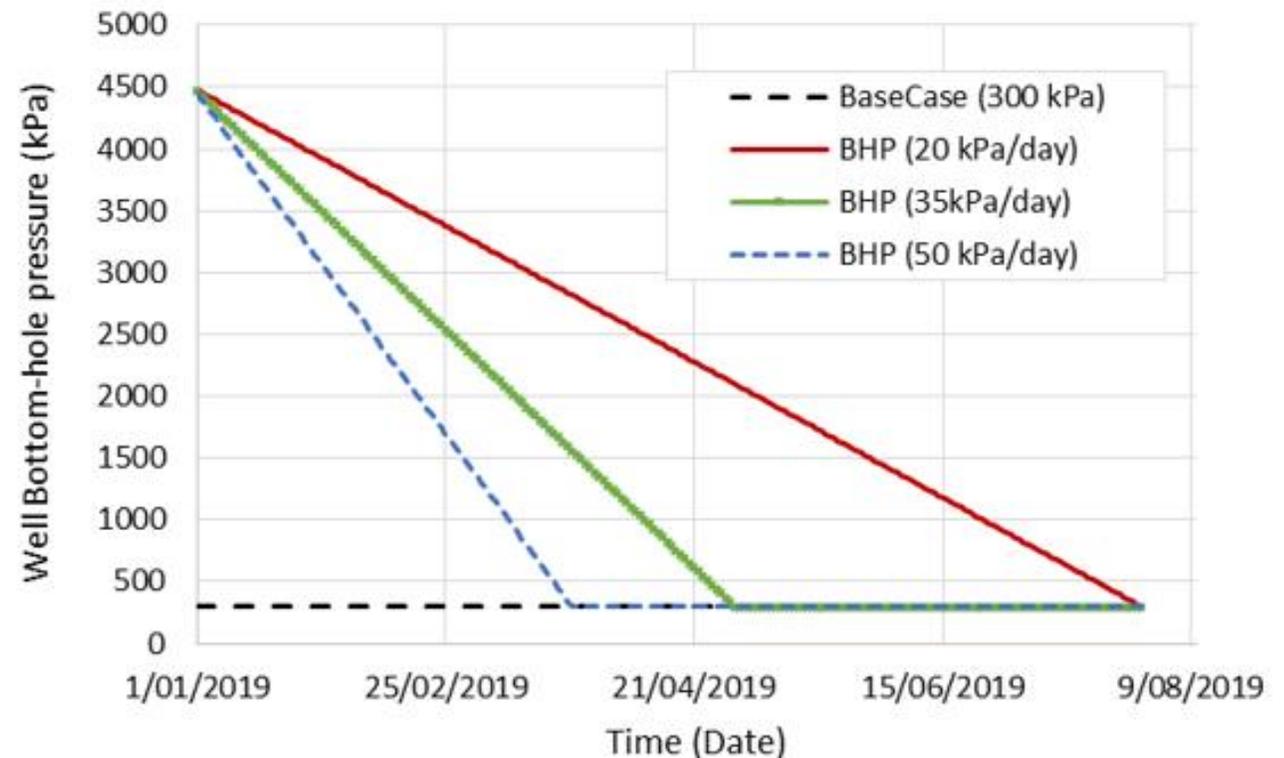
# Model Implementation

## ❖ Production Well Arrangements

**Table:** Proposed well completion and input properties

Parameter	Value
Grids well definition	1 1; 1
Production duration	20 years
Well radius (m)	0.0762
Skin	0
CH <sub>4</sub> mole fraction	1
Bottom-hole Pressure (kPa)	300 kPa

- ✓ Initially, the well is operated with a primary constraint of a **300 kPa** BHP as an immediate decline.
- ✓ For **gradual decline**, we modelled three rates of BHP drawdown (**20**, **35**, and **50 kPa/day**), as shown in the **Figure**.

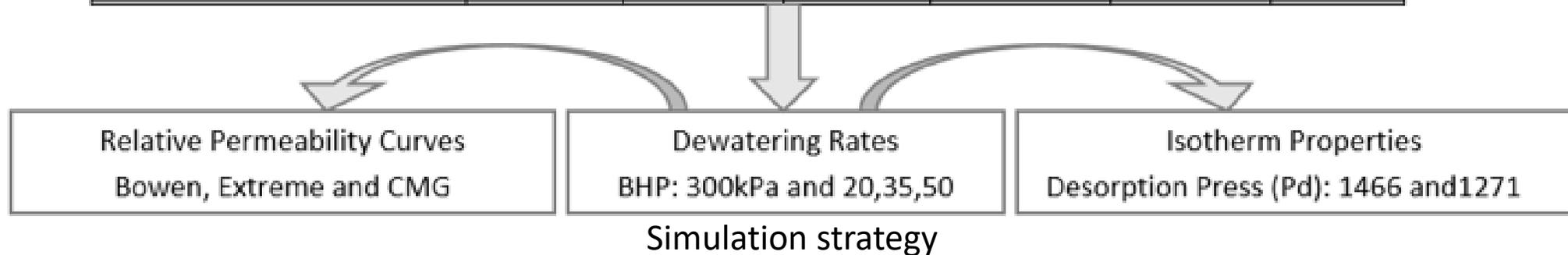


**Figure:** Immediate and gradual decline in well BHP

# Simulation Scenarios

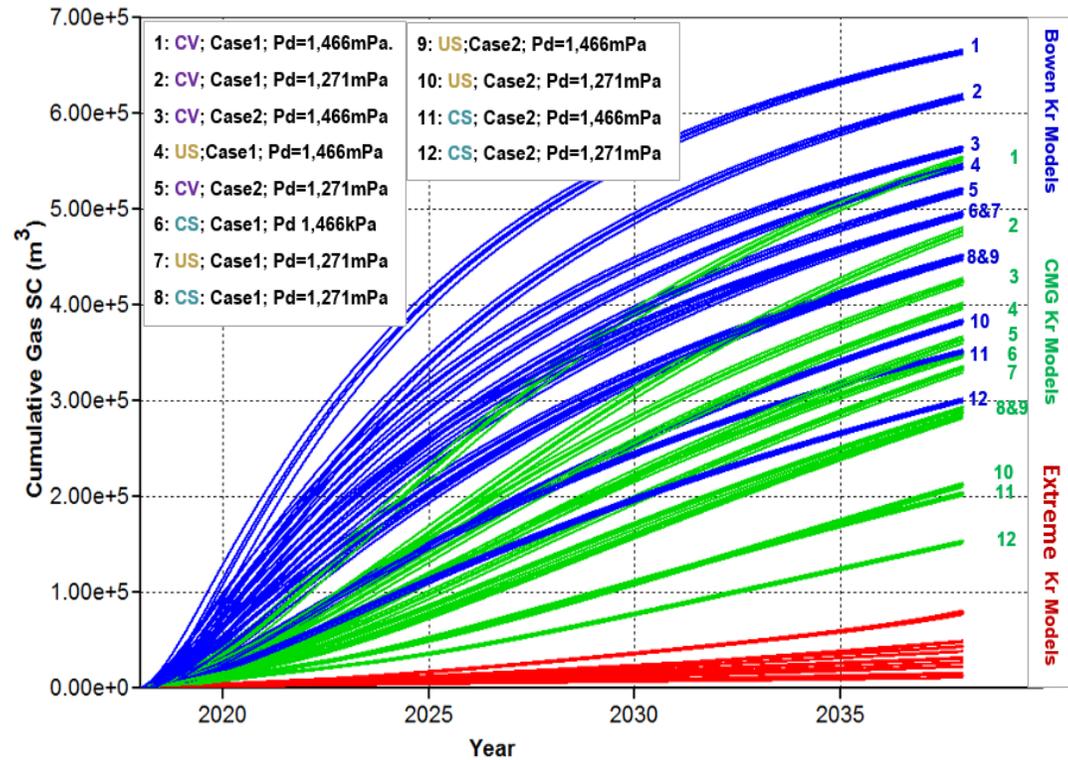
- Different case scenarios were systematically simulated for the whole matrix of conditions.
- A total of 144 ( $3 \times 4 \times 2 = 24$  runs for each case) separate runs were investigated for different drawdown scenarios.

Stress Conditions Versus Geomechanical properties	Constant volume (CV)		Constant stress (CS)		Uniaxial strain (US)	
	Case1	Case2	Case1	Case2	Case1	Case2
Poisson's Ratio, $\nu$	0.26	0.44	0.44	0.26	0.44	0.26
Young's Modulus, E (MPa)			3,528	2,072	3,528	2,072
Sorption-induced Strain, $\epsilon$	0.0151	0.0089			0.0151	0.0089

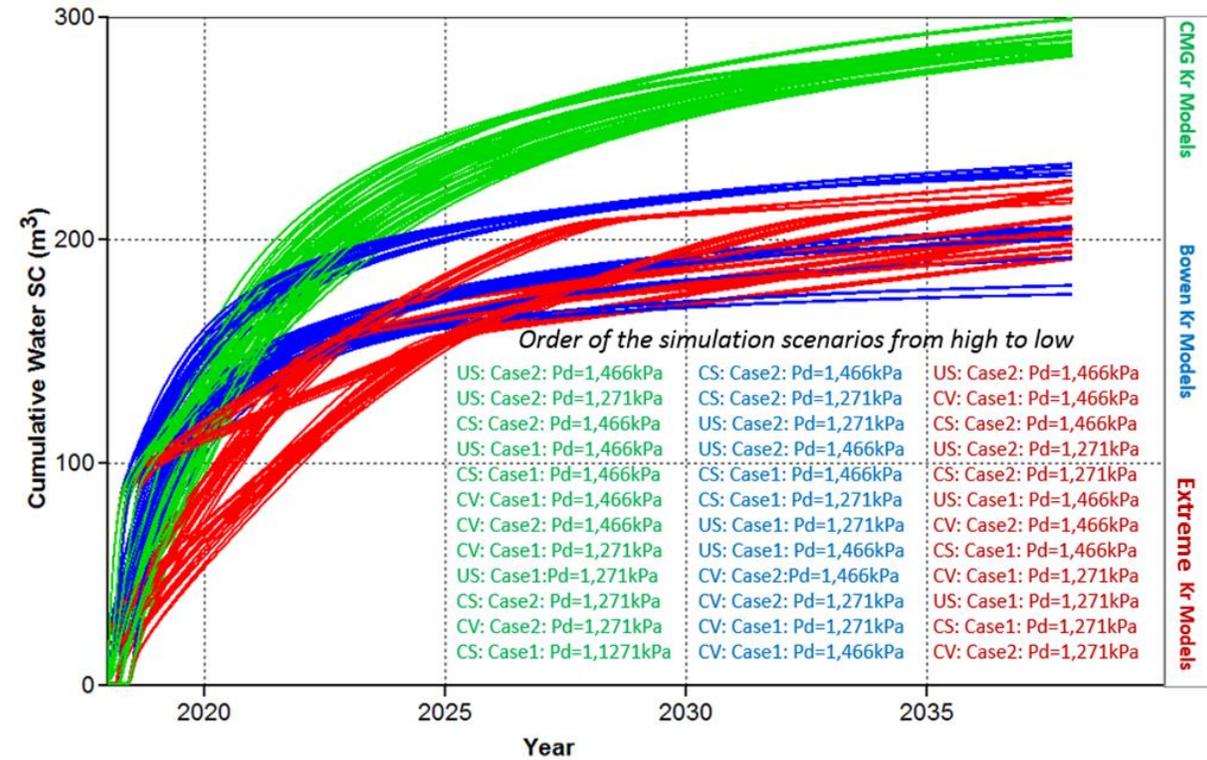


# Results and Analysis

## ❖ Cumulative Gas and Water Production Over 20 Years

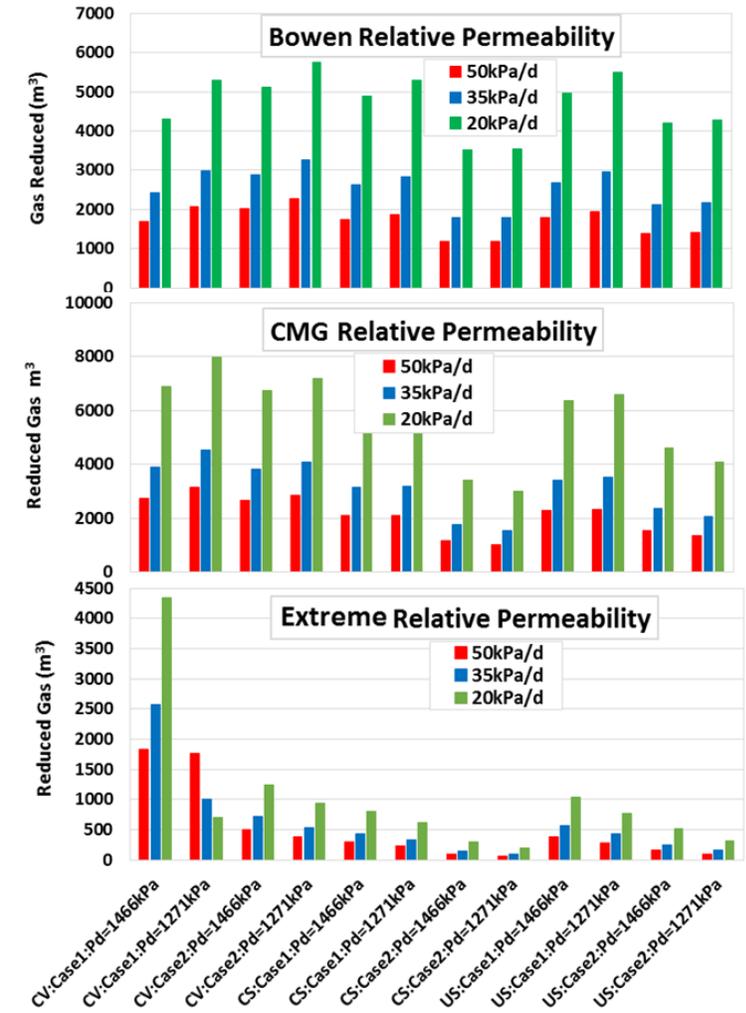
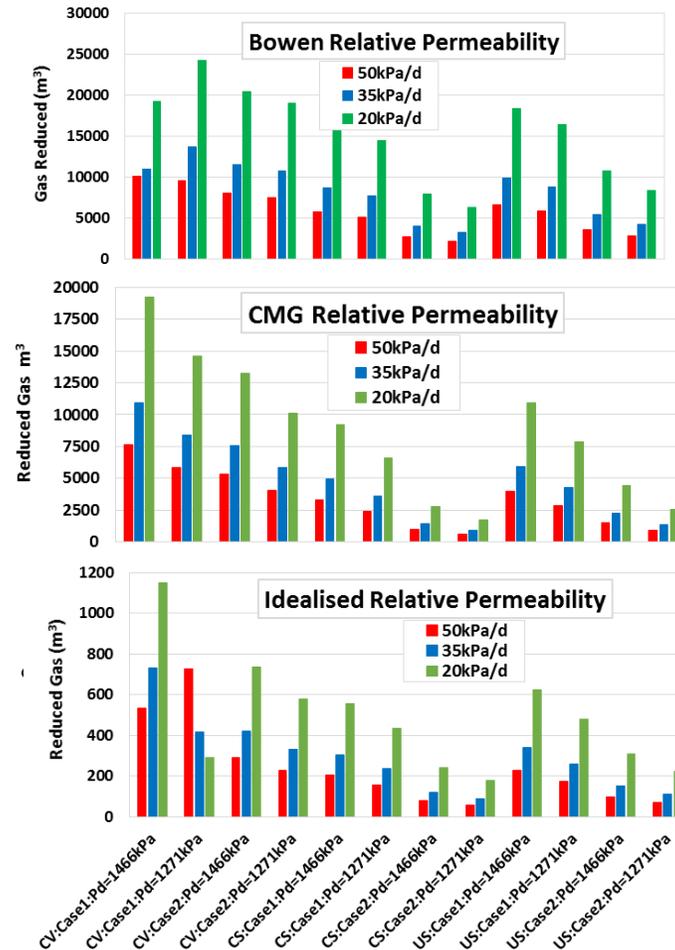
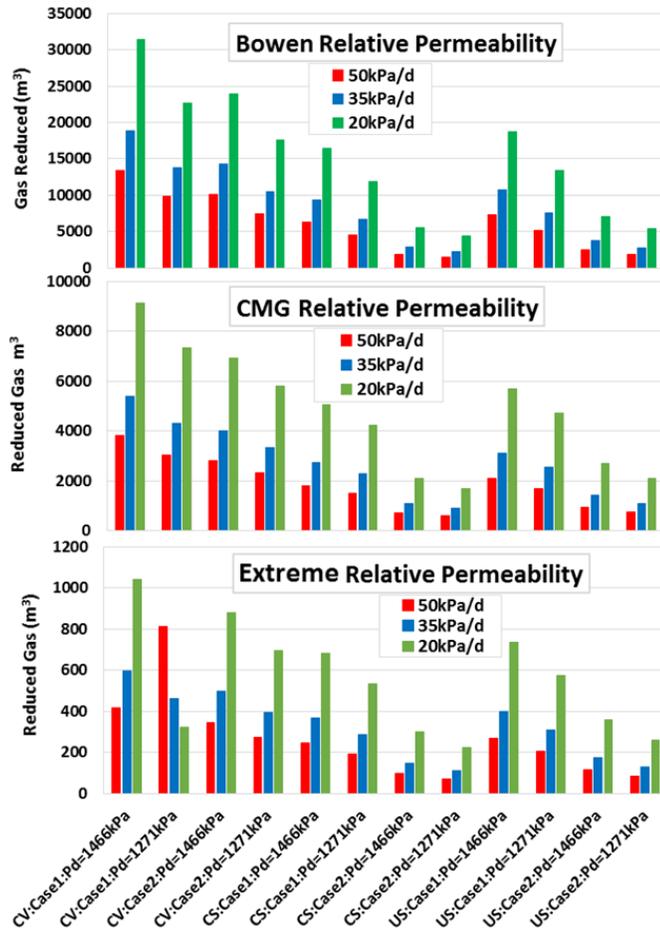


Cumulative gas production for different reservoir conditions under different dewatering rates over 20 years



Cumulative Water production for different reservoir conditions under different dewatering rates over 20 years

# Results and Analysis- Gas

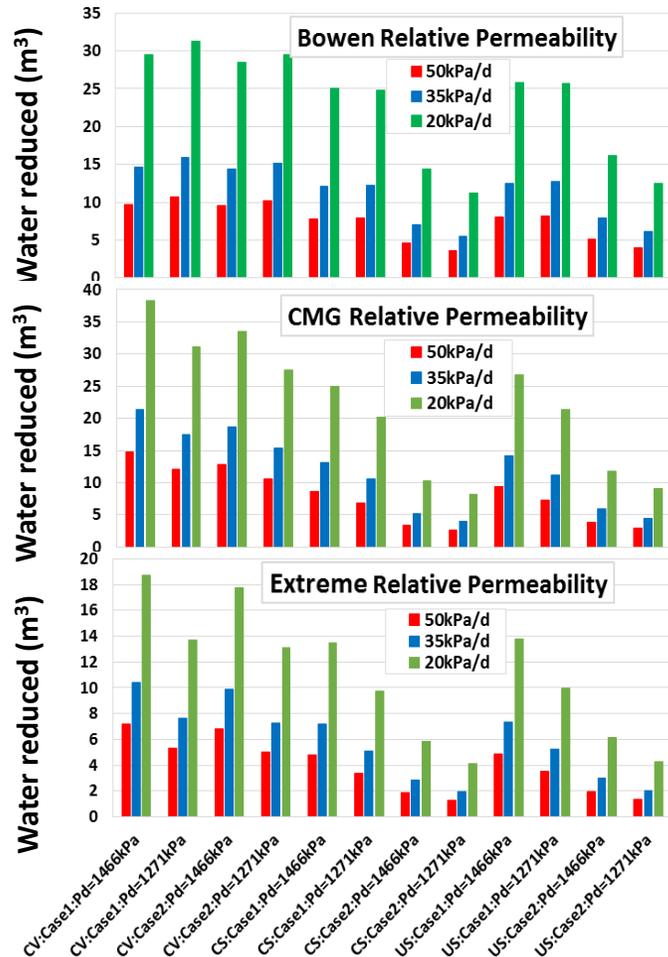


Gas reduction vs. BHP control after 1 year

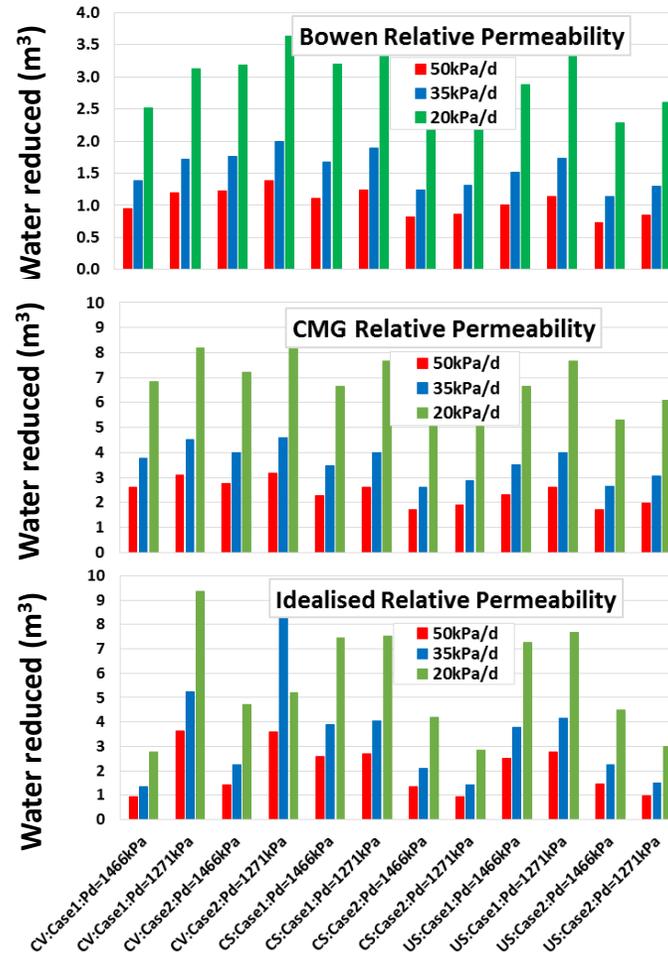
after 5 years

after 20 years

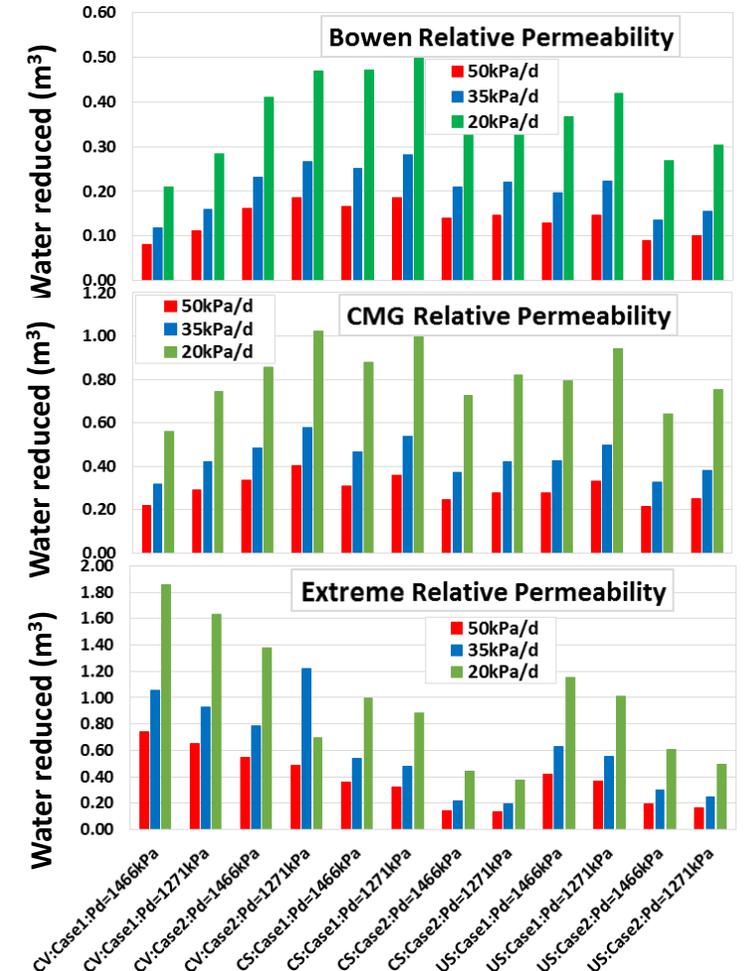
# Results and Analysis- Water



Water reduction vs. BHP control after 1 year



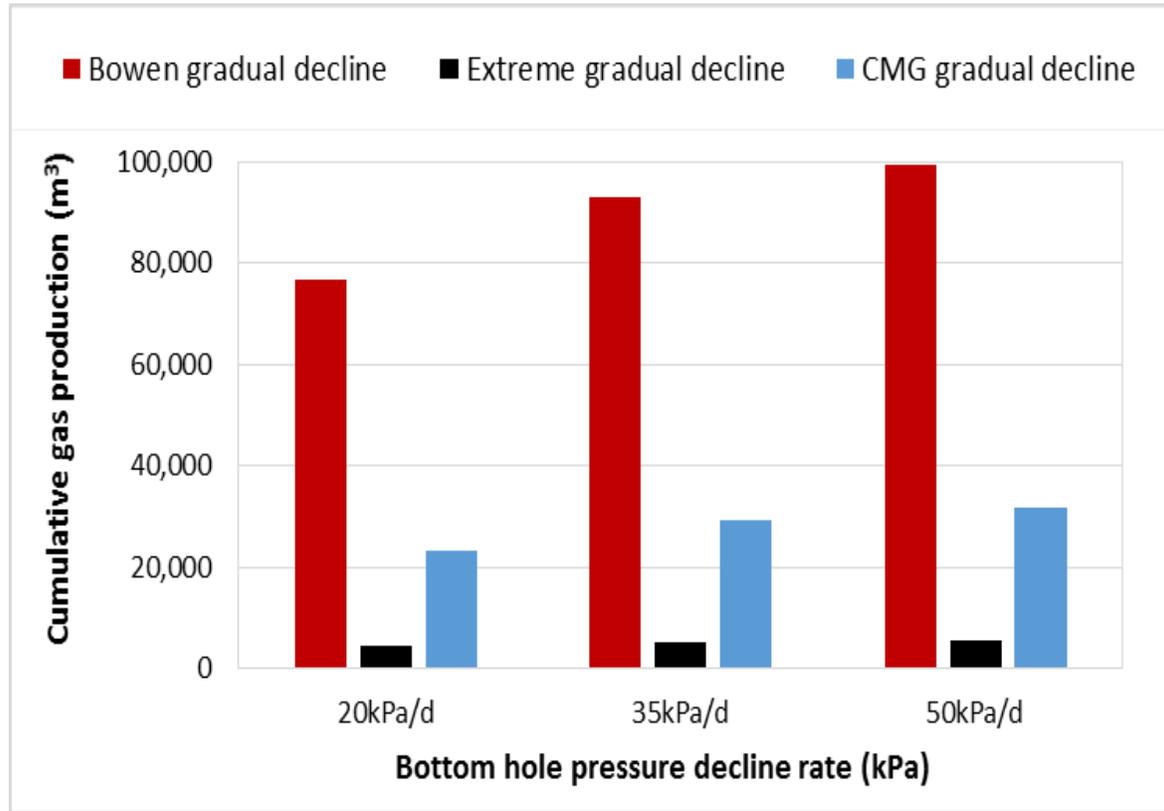
after 5 years



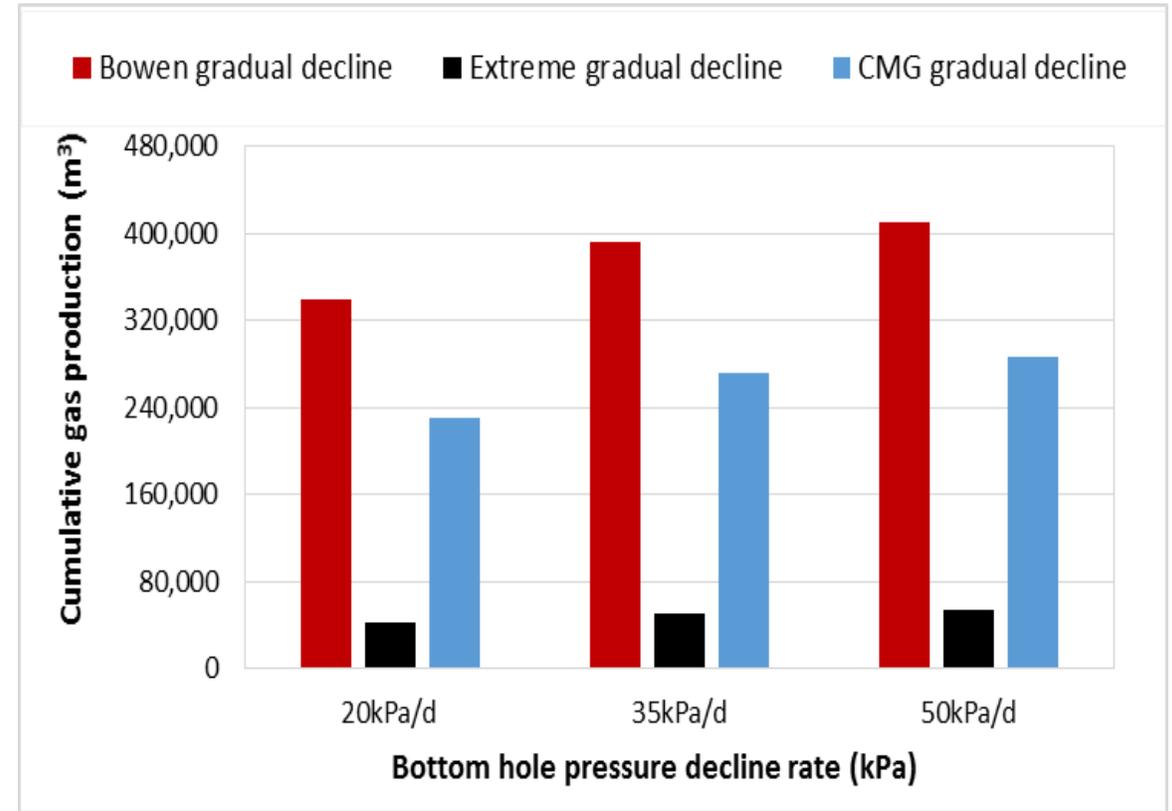
after 20 years

# Results and Analysis- Absolute Perm

**Ka=1 mD**



**Ka=10 mD**



# Conclusions

- ✓ Both absolute permeability changes and relative permeability curves have significant impact on dewatering efficiency and gas productivity behaviour.
- ✓ Under all the simulated scenarios, the lower the BHP the better gas production is achieved.

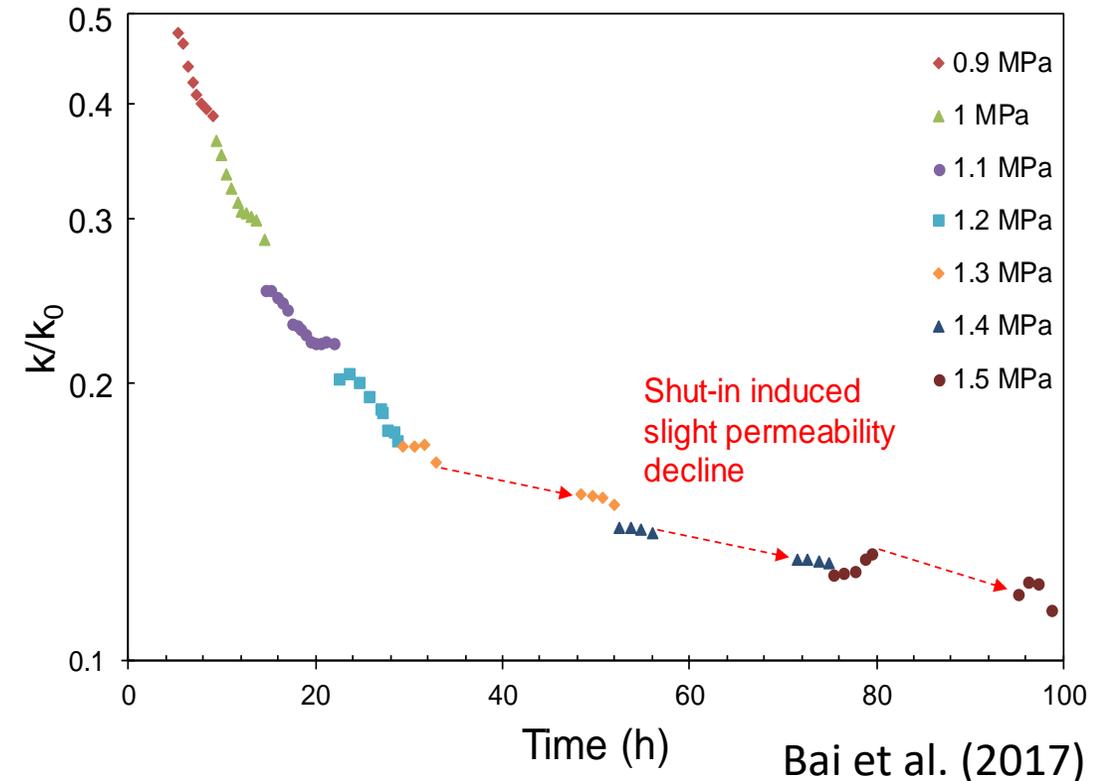
From an operating perspective, where subject to other constraints such as well stability and fines generation is excluded:

- ✓ There is no advantage to manage the BHP – other than to make it as low as possible and as quickly as possible.

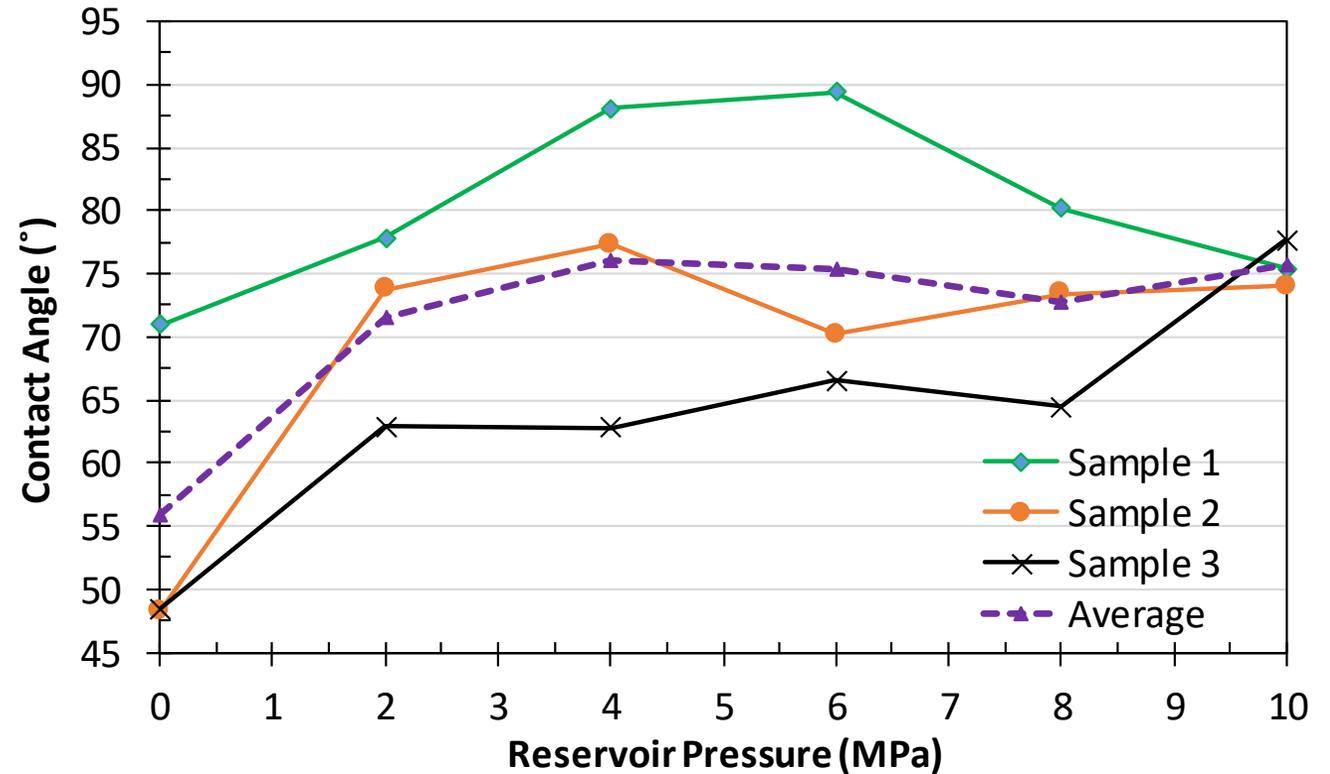
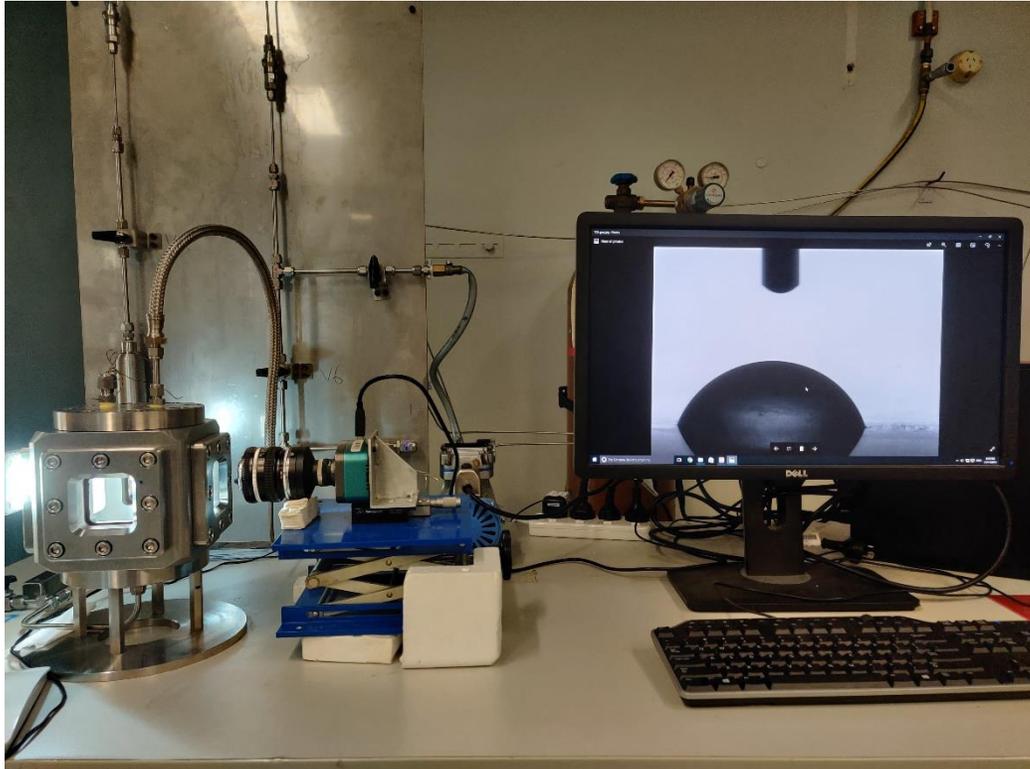
# Recommendations

This conclusion contradicts with some field observations that there may be benefits to be gained in terms of productivity in staging the reduction in BHP.

The possible reason(s) is that the work does not include any consideration of factors like the dynamic change of the intrinsic perm and relative perm, wellbore instability or fines generation from stress imbalances that may arise from rapid pressure changes.



# Recommendations- cont'd



- Coal becomes more hydrophilic (i.e. more wetting) during depletion

# Acknowledgments

We would like to acknowledge Arrow Energy for providing the financial support and the Computer Modelling Group (CMG) for providing the software licence to conduct this work.

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Thanks!  
Questions?