Figure 5: Single-phase results showing isolines of the mean reduction (nondimensionalised) of fracture permeability from a reference value.

 $\sigma_{\text{iso}}/h_{\text{ref}}$

 0.15

 0.20

 0.25

0.30

Figure 3: Elevation contour plot of a coal fracture surface obtained using digital optimal microscopy, highlighting smoothness between discontinuities.

The work focuses on the first stage of analysis, namely highfidelity modelling of two-phase flow in a single fracture.

- The lattice Boltzmann method (LBM) is used to resolve the hydrodynamics of fluid flow in rough fracture geometries.
- The LBM is well-established for use in porous media flows
- A phase-field model is employed to capture the interaction of two immiscible phases (i.e. water and gas), recovering a modified form of the Allen-Cahn equation.
- Recent modifications to the three-phase contact modelling improve the accuracy gas-water interactions at fracture walls Coal surfaces were imaged using Olympus DSX1000 digital optical microscope to generate roughness data.
- Two different lenses captured wide range of length scales
- An array of 10 x 10 sub-images stitched to create final image
- Power spectrum was extracted using 2D Fourier transform
- Power decay coefficient used to generate synthetic fractures Pressure gradients are applied to the models which predict fluid velocity, allowing permeability calculation.
- Permeability profile for single roughness and correlation follows a Gaussian distribution across many realisations • The dependence on roughness of the permeability mean and the standard deviation is non-linear \rightarrow requires advanced statistical modelling techniques \rightarrow Generalized additive model for location, scale and shape (GAMLSS)

Method

The absolute and relative permeability of a coal seam are key to production outcomes, including gas and water rates and reservoir compaction and subsidence. Contemporary model predictions typically use parameters sourced from downhole diagnostic tests and production history matching. However, this homogenises the influence of the cleat and fracture network, which is complex and somewhat random in nature. The concept of complementary relative permeability curves which smoothly vary with changing saturation has also been shown to be invalid in experimental and numerical studies. The variability and uncertainty associated with important modelling parameters translates to uncertainty in economic and environmental issues.

The aim of this research program is to develop

Figure 1: The top-down approach to be taken in this research is focused on analysis at three scales: (1) High-fidelity modelling of two-phase flow in a single

next-generation analysis tools to predict twophase flow at industry relevant scales in the subsurface, using stochastic analysis and upscaling of high-fidelity models of fracture flow.

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Introduction

Figure 4: Fractures are rough random surface surfaces, and parallel plate assumptions (i.e cubic law) do not hold. This influences interpreted aperture and resultant permeability at fracture and fracture network level. It is desirable to capture the influence of fracture geometry via distribution of expected behaviour.

Figure 6: Aspects of two-phase flow modelling in fractures showing (left) a rough fracture geometry and (right) random initialisation of water and gas.

0.1 0.9 0.2 0.5 Liquid saturation

The water and gas phases are initialised using a random distribution according to the prescribed saturation. A forcing term is applied driving the system to steady state and mimicking the pressure gradient. Having obtained the absolute permeability and expected flow rate from singlephase simulations, the relative permeability is calculated from steady-state average velocity values.

Two-phase flow in rough fractures

 0.10

Modelling has shown that (1) increased fracture roughness or decorrelation leads to increase in the standard deviation between results from different fracture realisations for both single- and twophase flows, and (2) the permeability of liquid and gas are nonlinearly dependent on saturation. Future work will apply this methodology to pressure driven flows to facilitate the generation of relative permeability curves and integration into DFN modelling.

Conclusions and Future Work

fracture using roughness statistics from digital optical microscopy and outputting surrogate model(s) linking flux, pressure and saturation based on hundreds of unique model realisations; (2) Transport in the discrete fracture network (DFN) of a representative elemental volume (REV) using fracture spacing and dispersion statistics from image logs and the surrogate model and statistics of two-phase flow in a single fracture, outputting averaged, orthotropic transport properties and statistics for each REV; (3) Integrated reservoir-geomechanical modelling using REV transport properties for multiple geological units and stratigraphy based on well logs and copula geostatistics, with feedback from production data and surface movement measurements from InSAR.

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Investigating the Relative Permeability of Coal Fractures Using Stochastic Analysis and High-Fidelity Computational Modelling

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 $\frac{8}{2}$

 $0.\overline{6}$

 $\overline{0}$

 0.2

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0.05

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Figure 2: Two-phase LBM simulation of oil displacing water in a CT scan of Berea sandstone fracture for validation purposes. Here blue and red mark oil and water phases correspondingly.

Figure 8: Graphs of (above) relative permeability and (below) number of liquid and gas in the steady state.